

afleiding wapening A_s

$$M_{Ed} = A_s f_{yd} \left(d - \frac{\beta_1 A_s f_{yd}}{b f_{cd} \alpha} x_u \right)$$

$$M_{Ed} = A_s f_{yd} \cdot d - \frac{\beta_1 A_s^2 f_{yd}^2}{b f_{cd} \alpha}$$

$$\frac{\beta_1 f_{yd}^2}{b f_{cd} \alpha} \cdot A_s^2 - f_{yd} \cdot d \cdot A_s + M_{Ed} = 0$$

$$A_s = f_{yd} \cdot d - \sqrt{(f_{yd} \cdot d)^2 - 4 \cdot \frac{\beta_1 f_{yd}^2}{b f_{cd} \alpha} \cdot M_{Ed}}$$

$$2 \cdot \frac{\beta_1 f_{yd}^2}{b f_{cd} \alpha}$$

afleiding x_u CBZ 01252 B beton

$$M_{Ed} = 2 b x_u f_{cd} (d - \beta x_u)$$

$$M_{Ed} = 2 b x_u f_{cd} \cdot d - 2 b x_u f_{cd} \beta x_u$$

$$\underbrace{2 b f_{cd} \beta}_{a} x_u^2 + \underbrace{(-2 b f_{cd} d)}_b x_u + \underbrace{M_{Ed}}_c$$

$$x_u = \frac{-b - \sqrt{b^2 - 4ac}}{2a} \quad \left(\text{oplossen via de kwadratische vergelijking} \right)$$

$$x_u = \frac{2 b f_{cd} d - \sqrt{(-2 b f_{cd} d)^2 - 4 \cdot 2 b f_{cd} \beta M_{Ed}}}{2 \cdot 2 b f_{cd} \beta}$$

$$x_u = \frac{2 b f_{cd} d}{2 \cdot 2 b f_{cd} \beta} - \sqrt{\frac{d^2 b^2 f_{cd}^2 d^2}{4 \cdot d^2 b^2 f_{cd}^2 \beta^2} - \frac{4 \cdot 2 b f_{cd} \beta \cdot M_{Ed}}{4 d^2 b^2 f_{cd}^2 \beta^2}}$$

$$x_u = \frac{d}{2\beta} - \sqrt{\frac{d^2}{(2\beta)^2} - \frac{M_{Ed}}{2 b f_{cd} \beta} \times \frac{4\beta}{4\beta}}$$

$$x_u = \frac{d}{2\beta} - \sqrt{\frac{d^2}{(2\beta)^2} - \frac{4\beta M_{Ed}}{2 b f_{cd} \cdot (2\beta)^2}}$$

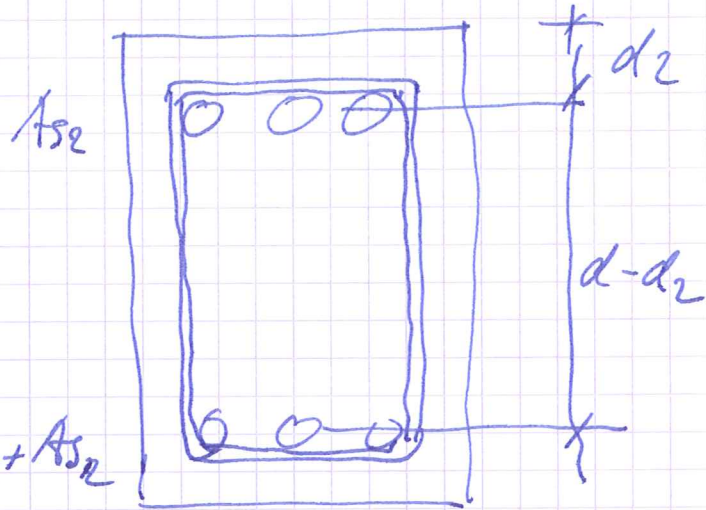
$$x_u = \frac{d - \sqrt{d^2 - \frac{4\beta M_{Ed}}{2 b f_{cd}}}}{2\beta}$$

2/7

Lebenwaarde M_{Ed}

Druckwäpung. ρ beton EC

Opneembaar M_{Ed}



Arch + druckwäpung

$$M_{Ed, \text{total}} = M_{Ed1} + M_{Ed2}$$

$$M_{Ed1} = A_{s1} \cdot f_{yd} \cdot z \quad A_{s1} + A_{s2}$$
$$= \rho_{\max} b d \cdot f_{yd} \cdot z$$

$$M_{Ed2} \Rightarrow M_{Ed, \text{total}} - M_{Ed1}$$

$$A_{s1} = \rho_{\max} \cdot b d$$

$$A_{s2} = \frac{M_{Ed2}}{f_{yd} (d - d_2)}$$

$$d_2 = d - \rho_{\text{druck}} \cdot d_{\text{bet}} - \frac{1}{2} d_{\text{gem, druck}}$$

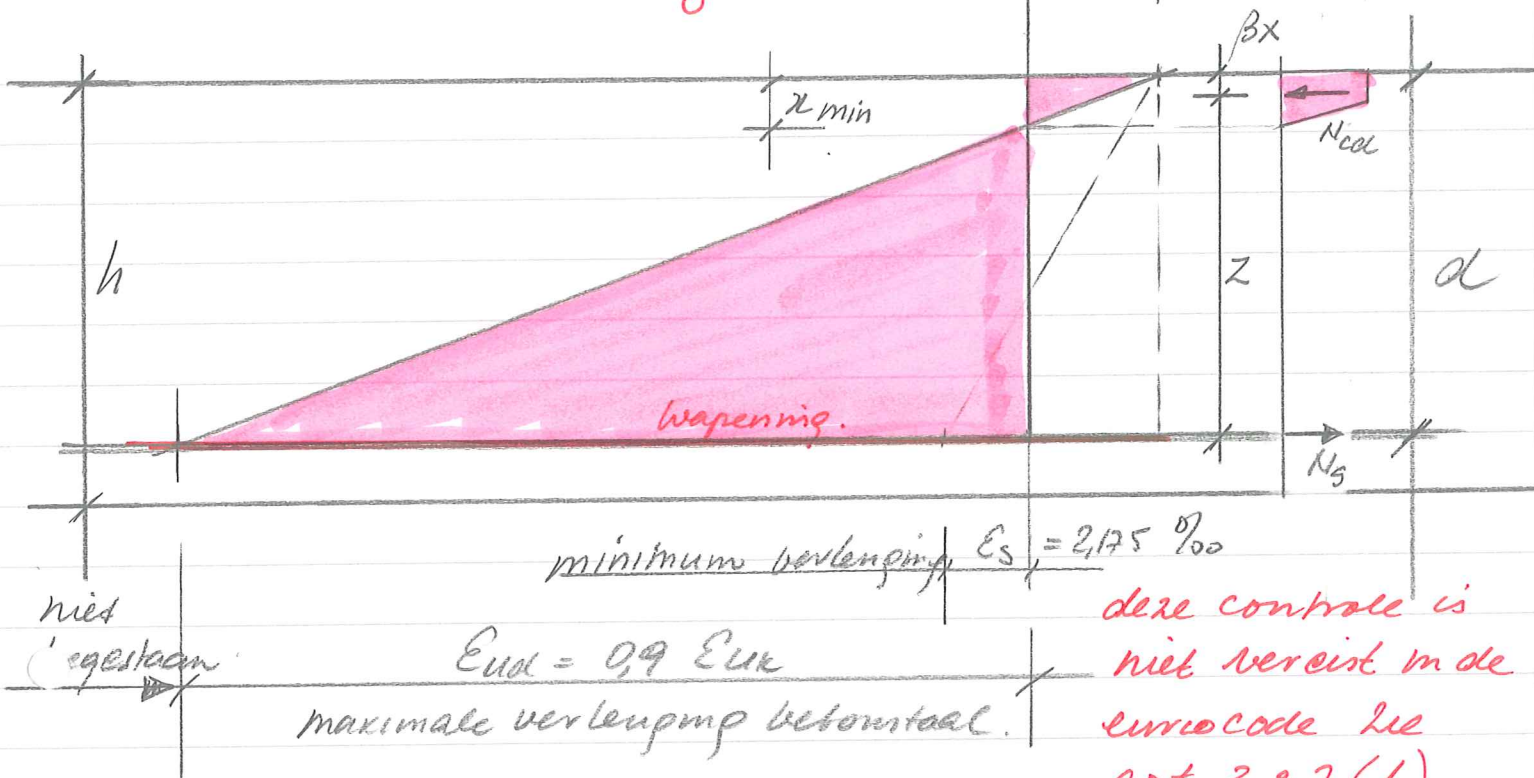
Archwäpung: $A_{s, \text{total}} = A_{s1} + A_{s2}$

druckwäpung: A_{s2}

Zie voorbeeld blz 61 CB 2

Beton buigwapening

B. beton E_c $\epsilon_{cu3} = 3,5 \text{ ‰}$ f_{cd}



minimum verlenging $E_s = 2,175 \text{ ‰}$

$E_{ud} = 0,9 E_{uk}$
maximale verlenging betonstaal.

deze controle is niet vereist in de eurocode 2 zie art 3.2.7 (b)

$$\frac{x_{min}}{E_{cu3}} = \frac{d}{E_{ud} + E_{cu3}} \Rightarrow x_{min} = \frac{E_{cu3}}{E_{ud} + E_{cu3}} \cdot d$$

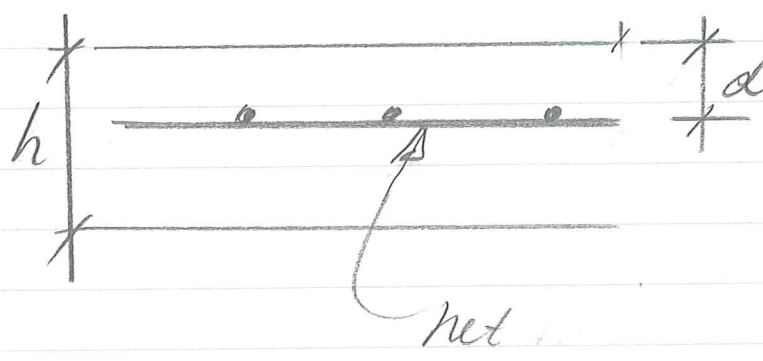
$$N_{cd} = \alpha \cdot b \cdot x \cdot f_{cd} \quad A_s = N_{cd} / f_{yd}$$

$$z = d - \beta x \quad M_{ud} = N_{cd} \cdot z$$

ongeseheurde doorsnede $W_c = 1/6 \cdot b \cdot h^2$

trekspanning in beton $f_{ctm} \times \left(116 - \frac{h}{1000}\right)$ $h \leq 600$

Scheurmoment $M_{rel,c} = W_c \cdot f_{ctm}$



dus van de totale beton doorsnede.

B beton E2

SCHNITTSTÄRKE: $M_r = W_c \cdot f_{ctm} \cdot \left(1,6 - \frac{h}{1000}\right)$

$$A_{min} = \frac{M_r}{2 \cdot f_{yk}} = \frac{\frac{1}{6} b h^2 \cdot f_{ctm}}{2 \cdot f_{yk}}$$

Neutrale Faser: $z = 0,9 d$
 $d = 0,9 h$

$$= \frac{\frac{1}{6} \cdot b h^2 \cdot f_{ctm}}{0,81 h \cdot f_{yk}}$$

$$= \frac{b \cdot d}{b \cdot 0,81 \cdot 0,9} \cdot \frac{f_{ctm}}{f_{yk}}$$

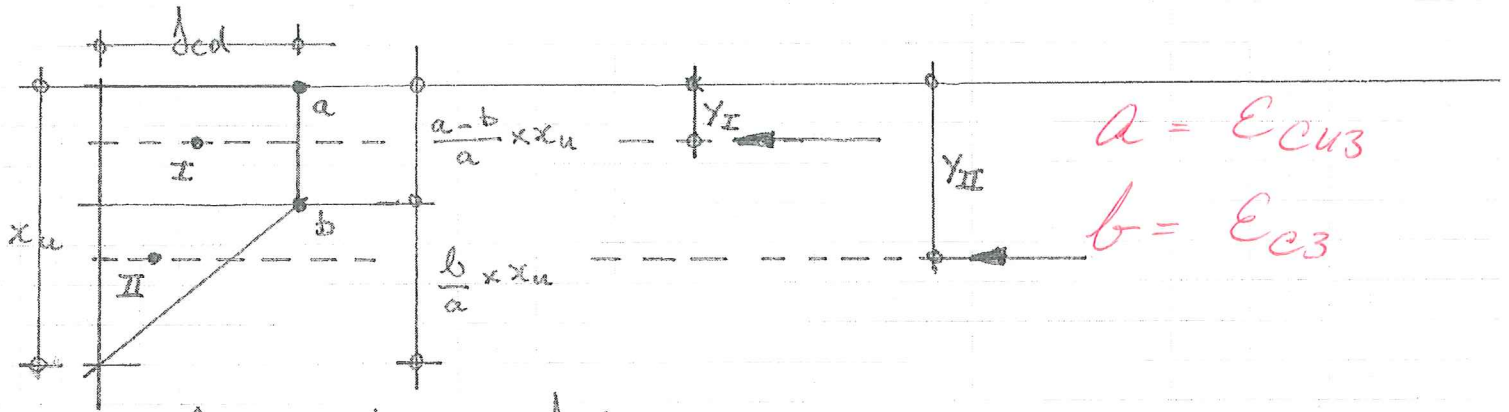
$$= 0,23 b d$$

Für Berechnung Minimum Bewehrung.

Ableitung Minimum Bewehrung in EB2

= Benadernungsformule!
 $z = 0,81 h$

Doorsnede berekening beton - bepaling α en β - Eurocode 2



$a = \epsilon_{cu3}$
 $b = \epsilon_{c3}$

$$\left. \begin{aligned} A_I &= \frac{a-b}{a} \times x_u \times d \\ A_{II} &= \frac{1}{2} \times \frac{b}{a} \times x_u \times d \end{aligned} \right\} \epsilon A = \left[\frac{a-b}{a} + \frac{b}{2a} \right] \times x_u \times d$$

$$= \frac{2a-b}{2a} \times x_u \times d$$

$\Rightarrow \alpha = \frac{2a-b}{2a}$

$y_I = \frac{1}{2} \times \frac{a-b}{a} \times x_u = \frac{a-b}{2a} \times x_u$

$y_{II} = \left[\frac{a-b}{a} + \frac{1}{3} \frac{b}{a} \right] \times x_u = \frac{a - \frac{2}{3}b}{a} \times x_u$

$\alpha = \frac{a - \frac{b}{2}}{a}$

$A_I \times y_I = \frac{a-b}{a} \times \frac{a-b}{2a} \times x_u^2 \times d = \frac{(a-b)^2}{2a^2} \times x_u^2 \times d$

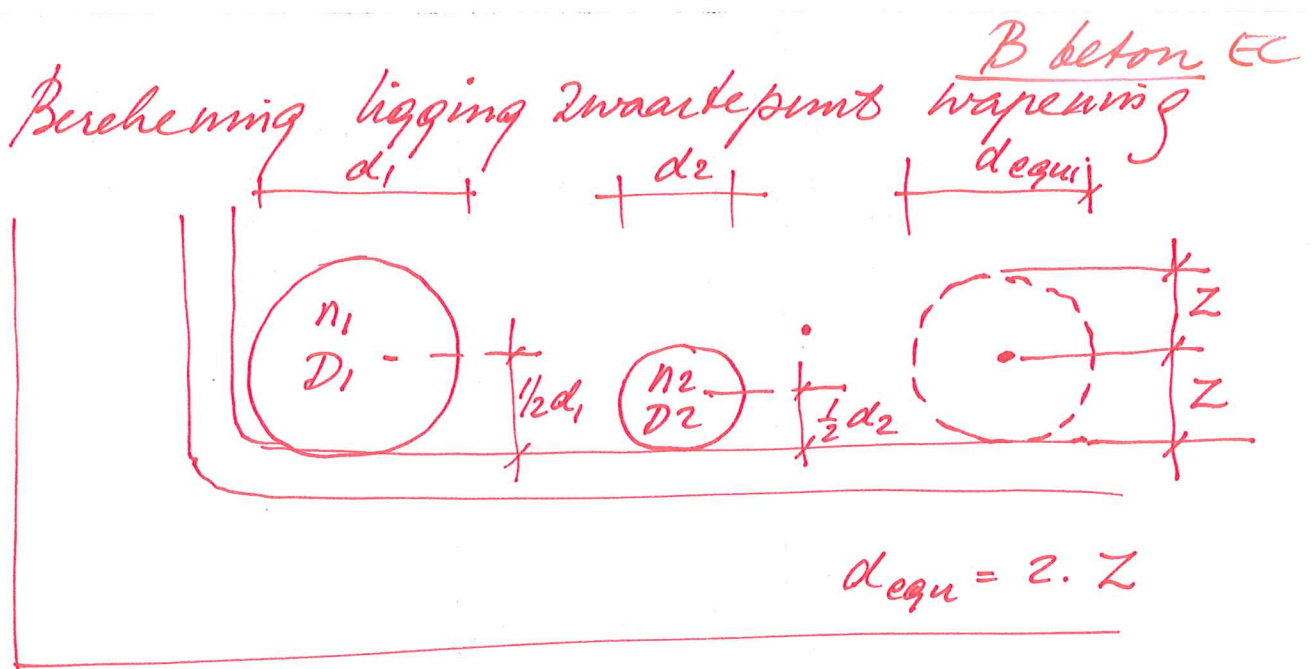
$A_{II} \times y_{II} = \frac{b}{2a} \times \frac{a - \frac{2}{3}b}{a} \times x_u^2 \times d = \frac{ab - \frac{2}{3}b^2}{2a^2} \times x_u^2 \times d$

$\Sigma (A \times y) = \frac{(a-b)^2}{2a^2} + \frac{ab - \frac{2}{3}b^2}{2a^2} = \frac{a^2 - 2ab + b^2 + ab - \frac{2}{3}b^2}{2a^2} \times x_u^2 \times d$

$= \frac{a^2 - ab + \frac{1}{3}b^2}{2a^2} \times x_u^2 \times d$

$\frac{\Sigma (A \times y)}{\Sigma A} = \frac{\frac{a^2 - ab + \frac{1}{3}b^2}{2a^2} \times x_u^2 \times d}{\frac{2a-b}{2a} \times x_u \times d} = \frac{a^2 - ab + \frac{1}{3}b^2}{2a^2 - ab} \times x_u$

$\Rightarrow \beta = \frac{a^2 - ab + \frac{1}{3}b^2}{2a^2 - ab}$

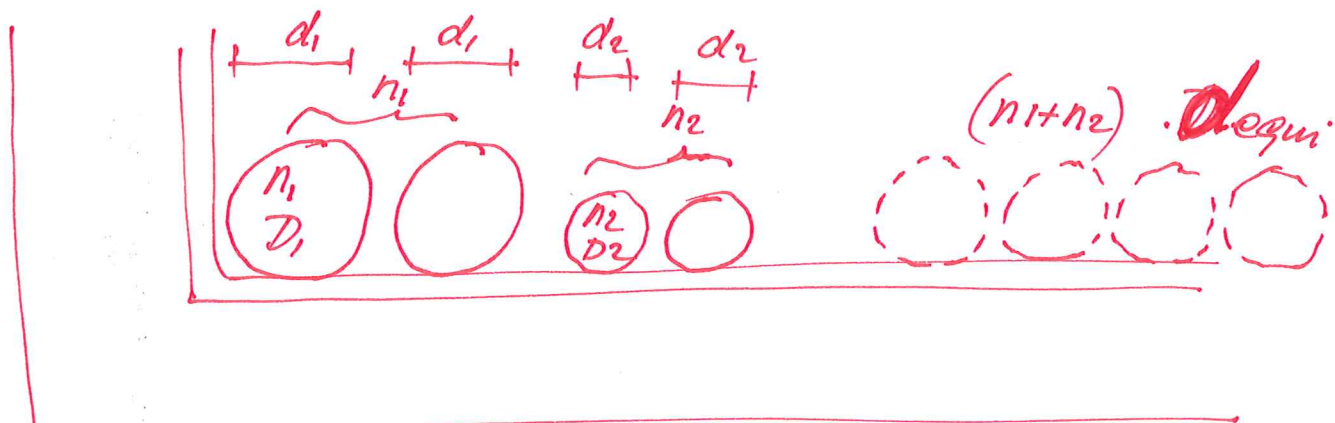


$$Z = \frac{n_1 D_1 \cdot \frac{1}{2} d_1 + n_2 D_2 \cdot \frac{1}{2} d_2}{n_1 D_1 + n_2 D_2}$$

te gebruiken voor berekening nutstige hoogte.

Berekening equivalente diameter voor bijvoorbeeld verankering, scheurwijdte e.d.

wordt verder niet gebruikt.



$$n_1 D_1 + n_2 D_2 = (n_1 + n_2) \cdot D_{equi} \Rightarrow D_{equi} = \frac{n_1 D_1 + n_2 D_2}{n_1 + n_2}$$

$$D_{equi} = \frac{1}{4} \cdot \pi \cdot d_{equi}^2 \quad d_{equi} = \sqrt{\frac{4 \cdot D_{equi}}{\pi}}$$

$$d_{equi} = \sqrt{\frac{4 \cdot (n_1 D_1 + n_2 D_2)}{\pi \cdot (n_1 + n_2)}}$$

echter

verankering lengte : enkele staaf : geen equivalent.
 scheurwijdte : gemiddelde diameter :